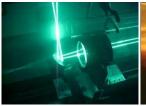
Computer graphics III – Light reflection, BRDF

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Recap – Basic radiometric quantities

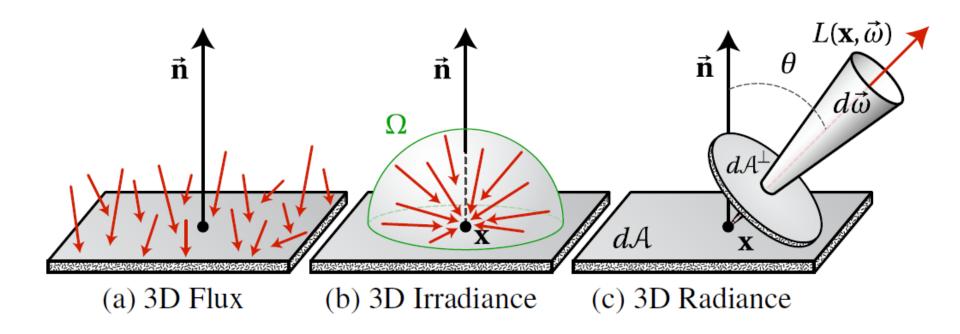


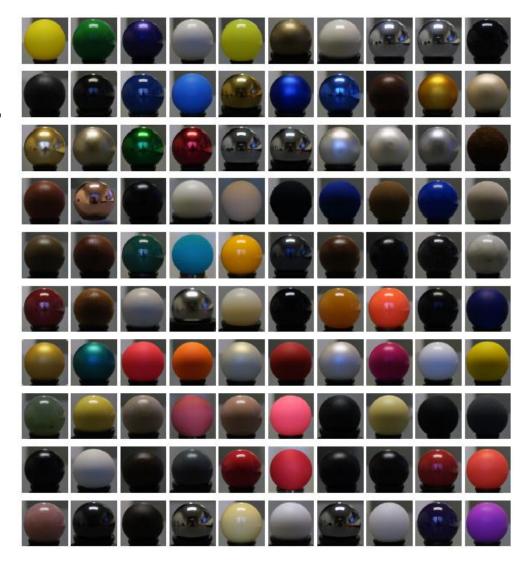
Image: Wojciech Jarosz

Interaction of light with a surface

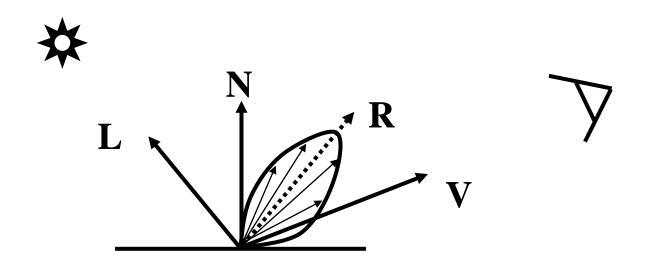
- Absorption
- Reflection
- Transmission / refraction
- Reflective properties of materials determine
 - the relation of **reflected** radiance L_r to **incoming** radiance L_i , and therefore
 - the appearance of the object: color, glossiness, etc.

Interaction of light with a surface

- Same illumination
- Different materials

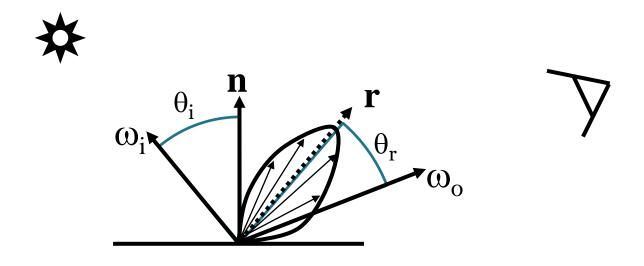


Recall the Phong shading model



$$C = I\left(k_d(N \cdot L) + k_s(V \cdot R)^n\right)$$
$$R = 2(N \cdot L)N - L$$

I) Adopt radiometric notation



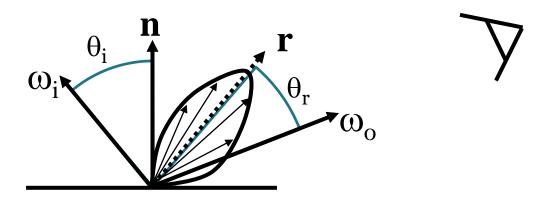
$$L_{o}(\omega_{o}) = L_{i}(\omega_{i}) \left(k_{d} \cos \theta_{i} + k_{s} \cos^{n} \theta_{r} \right)$$

$$\cos \theta_r = \omega_o \cdot \mathbf{r} \qquad \mathbf{r} = 2(\mathbf{n} \cdot \omega_i) \mathbf{n} - \omega_i$$

Exact same thing as on the previous slide – just using physically-based notation.

BRDF corresponding to the original Phong shading model





BRDF:
$$f_r = \frac{L_o}{L_i \cos \theta_i}$$

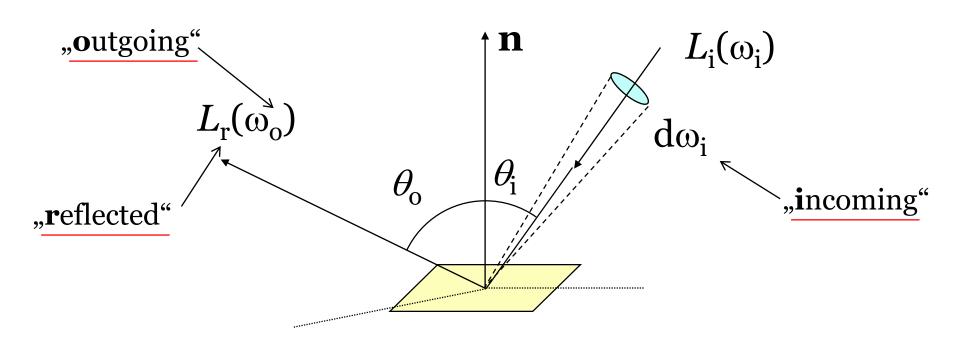
General definition of a BRDF

$$f_r^{Phong Orig} = k_d + k_s \frac{\cos^n \theta_r}{\cos \theta_i}$$

Application of this definition to the Phong shading formula.

BRDF – Formal definition

Bidirectional Reflectance Distribution Function



$$f_r(\omega_i \to \omega_o) = \frac{dL_r(\omega_o)}{L_i(\omega_i) \cdot \cos \theta_i \cdot d\omega_i} \quad [sr^{-1}]$$

BRDF

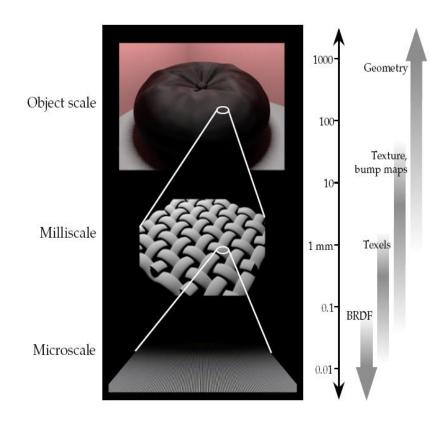
 Mathematical model of the reflection properties of a surface

- Intuition
 - Value of a BRDF = probability density, describing the event that a light energy "packet", or "photon", coming from direction ω_i gets reflected to the direction ω_o .
- Range:

$$f_r(\omega_i \to \omega_o) \in [0, \infty)$$

BRDF

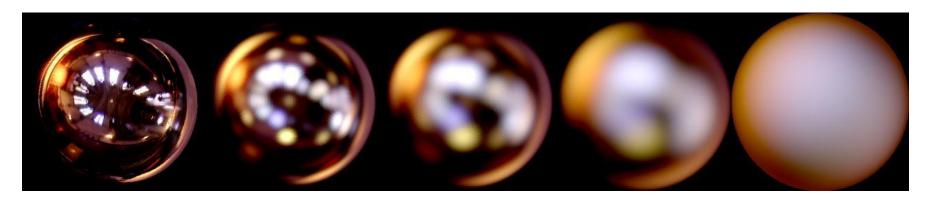
 The BRDF is a model of the bulk behavior of light on the microstructure when viewed from distance



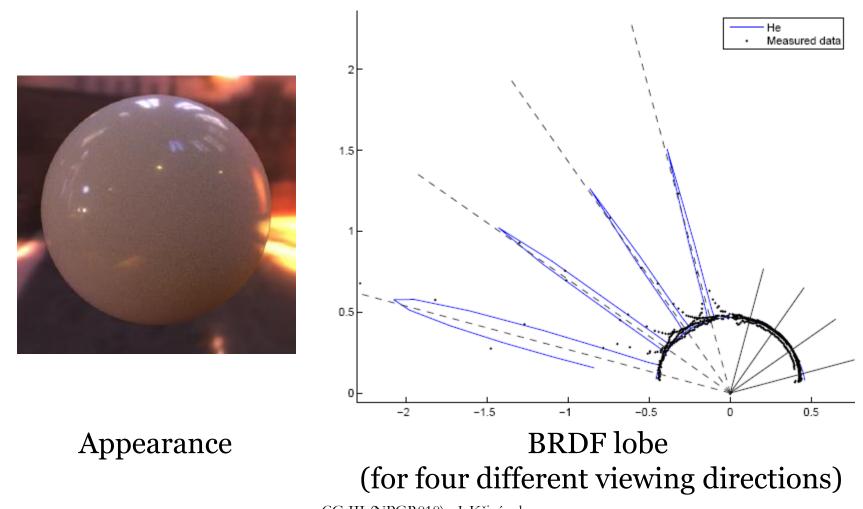
VIDEO ZOOMING INTO A MATERIAL

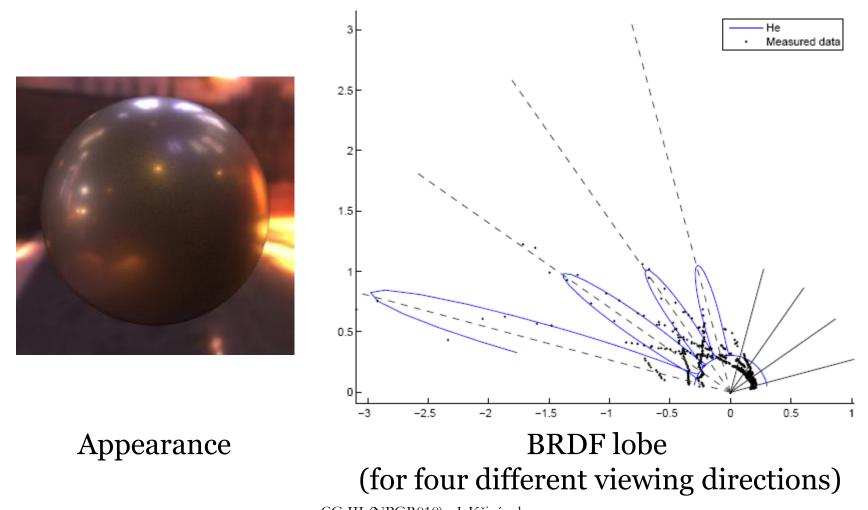
Surface roughness and blurred reflections

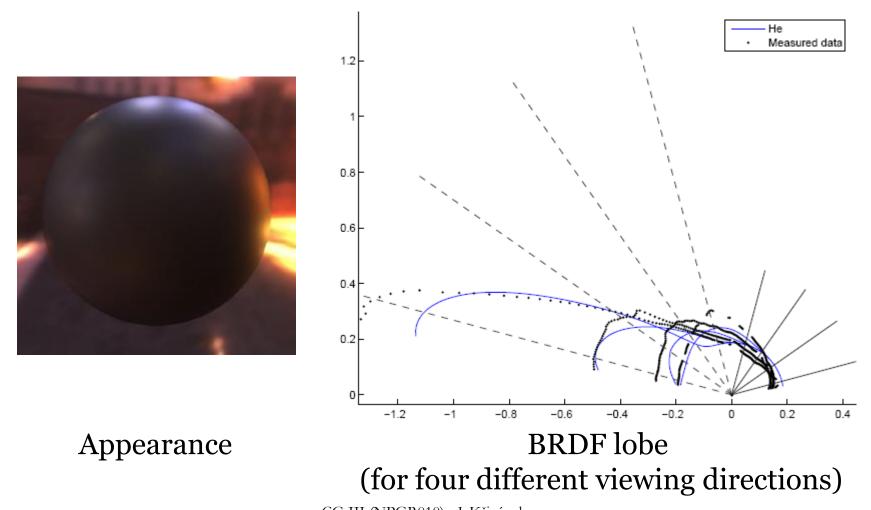
The rougher the blurrier

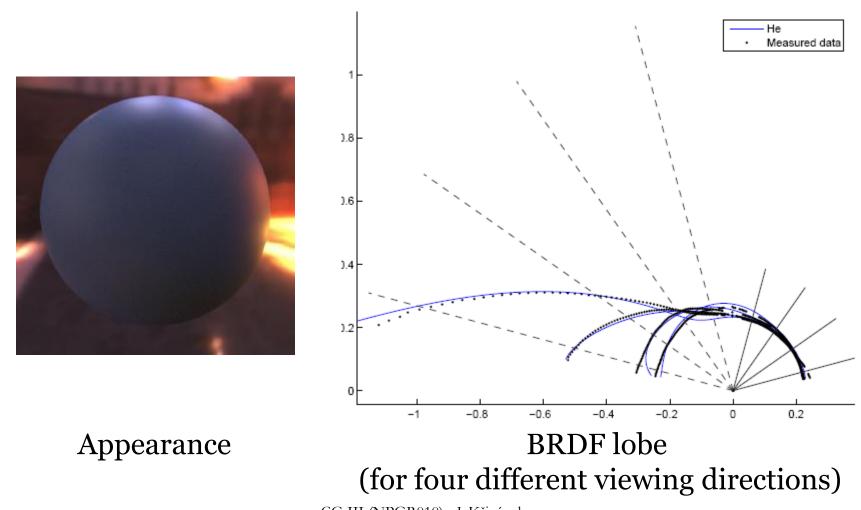


Microscopic surface roughness





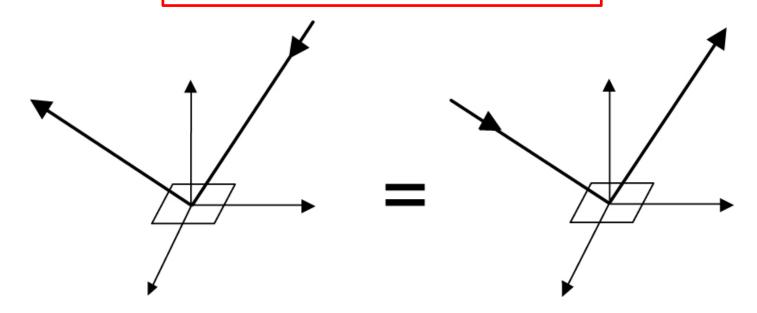




BRDF properties

 Helmholz reciprocity (always holds in nature, a physically-plausible BRDF model must follow it)

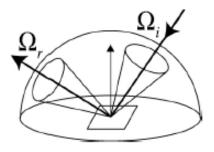
$$f_r(\omega_i \to \omega_o) = f_r(\omega_o \to \omega_i)$$



BRDF properties

Energy conservation

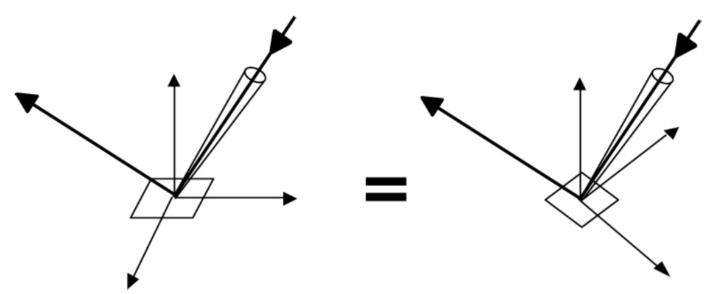
 A patch of surface cannot reflect more light energy than it receives



BRDF (an)isotropy

■ **Isotropic BRDF** = invariant to a rotation around surface normal

$$f_r(\theta_i, \phi_i; \theta_o, \phi_o) = f_r(\theta_i, \phi_i + \phi; \theta_o, \phi_o + \phi)$$
$$= f_r(\theta_i, \theta_o, \phi_o, \phi_o - \phi_i)$$



Surfaces with anisotropic BRDF



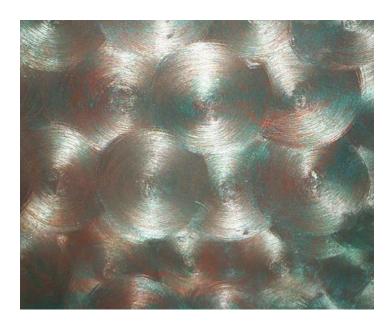
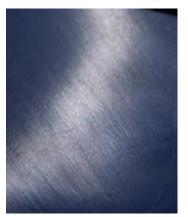
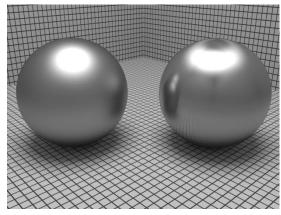


Figure 9: Anisotropic Aluminum Wheel





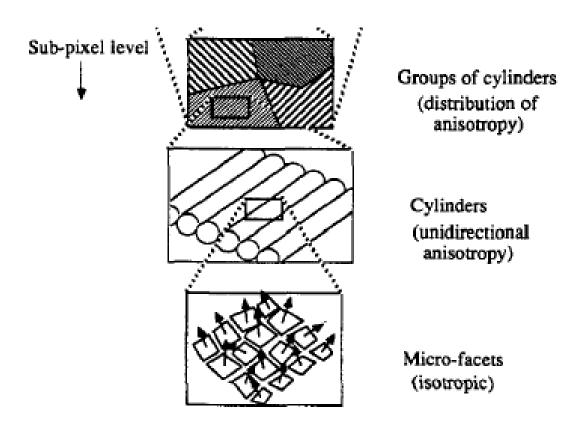




fibers

Anisotropic BRDF

 Different microscopic roughness in different directions (brushed metals, fabrics, ...)



Isotropic vs. anisotropic BRDF

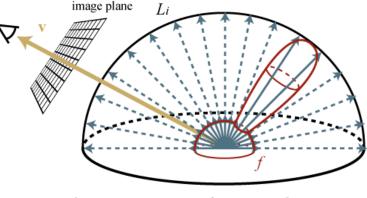
- **Isotropic** BRDFs have only 3 degrees of freedom
 - □ Instead of ϕ_i and ϕ_o it is enough to consider only $\Delta \phi = \phi_i \phi_o$
 - But this is not enough to describe an anisotropic BRDF
- Description of an anisotropic BRDF
 - ϕ_i and ϕ_o are expressed in a **local coordinate frame** (U, V, N)
 - *U* ... tangent e.g. the direction of brushing
 - V... binormal
 - N... surface normal ... the Z axis of the local coordinate frame

Reflection equation

- A.k.a. reflectance equation, illumination integral,
 OVTIGRE ("outgoing, vacuum, time-invariant, gray radiance equation")
- "How much **total** light gets reflected in the direction ω_o ?"
- From the definition of the BRDF, we have

$$dL_{r}(\omega_{o}) = f_{r}(\omega_{i} \to \omega_{o}) \cdot L_{i}(\omega_{i}) \cdot \cos \theta_{i} d\omega_{i}$$

Reflection equation



 Total reflected radiance: integrate contributions of incident radiance, weighted by the BRDF, over the hemisphere

$$L_{\rm r}(\omega_{\rm o}) = \int_{H({\bf x})} L_{\rm i}(\omega_{\rm i}) \cdot f_{r}(\omega_{\rm i} \to \omega_{\rm o}) \cdot \cos\theta_{\rm i} \; \mathrm{d}\omega_{\rm i}$$
 upper hemisphere over x



$$=\int$$



FIX THIS

Reflection equation

- Evaluating the reflectance equation renders images!!!
 - Direct illumination
 - Environment maps
 - Area light sources
 - etc.

Energy conservation – More rigorous

 Reflected flux per unit area (i.e. radiosity *B*) cannot be larger than the incoming flux per unit surface area (i.e. irradiance *E*).

$$\frac{B}{E} = \frac{\int L_r(\omega_o) \cos \theta_o \, d\omega_o}{\int L_i(\omega_i) \cos \theta_i \, d\omega_i} = \frac{\int \left[\int f_r(\omega_i \to \omega_o) L_i(\omega_i) \cos \theta_i \, d\omega_i\right] \cos \theta_o \, d\omega_o}{\int L_i(\omega_i) \cos \theta_i \, d\omega_i} = \frac{\int L_i(\omega_i) \cos \theta_i \, d\omega_i}{\int L_i(\omega_i) \cos \theta_i \, d\omega_i} = \frac{\int \left[\int f_r(\omega_i \to \omega_o) L_i(\omega_i) \cos \theta_i \, d\omega_i\right] \cos \theta_o \, d\omega_o}{\int L_i(\omega_i) \cos \theta_i \, d\omega_i} = \frac{\int \left[\int f_r(\omega_i \to \omega_o) L_i(\omega_i) \cos \theta_i \, d\omega_i\right] \cos \theta_o \, d\omega_o}{\int L_i(\omega_i) \cos \theta_i \, d\omega_i} = \frac{\int \left[\int f_r(\omega_i \to \omega_o) L_i(\omega_i) \cos \theta_i \, d\omega_i\right] \cos \theta_o \, d\omega_o}{\int L_i(\omega_i) \cos \theta_i \, d\omega_i} = \frac{\int \left[\int f_r(\omega_i \to \omega_o) L_i(\omega_i) \cos \theta_i \, d\omega_i\right] \cos \theta_o \, d\omega_o}{\int L_i(\omega_i) \cos \theta_i \, d\omega_i} = \frac{\int \left[\int f_r(\omega_i \to \omega_o) L_i(\omega_i) \cos \theta_i \, d\omega_i\right] \cos \theta_o \, d\omega_o}{\int L_i(\omega_i) \cos \theta_i \, d\omega_i} = \frac{\int \left[\int f_r(\omega_i \to \omega_o) L_i(\omega_i) \cos \theta_i \, d\omega_i\right] \cos \theta_o \, d\omega_o}{\int L_i(\omega_i) \cos \theta_i \, d\omega_i} = \frac{\int \left[\int f_r(\omega_i \to \omega_o) L_i(\omega_i) \cos \theta_i \, d\omega_i\right] \cos \theta_o \, d\omega_o}{\int L_i(\omega_i) \cos \theta_i \, d\omega_i} = \frac{\int \left[\int f_r(\omega_i \to \omega_o) L_i(\omega_i) \cos \theta_i \, d\omega_i\right] \cos \theta_o \, d\omega_o}{\int L_i(\omega_i) \cos \theta_i \, d\omega_i} = \frac{\int \left[\int f_r(\omega_i \to \omega_o) L_i(\omega_i) \cos \theta_i \, d\omega_i\right] \cos \theta_o \, d\omega_o}{\int \int \int f_r(\omega_i \to \omega_o) L_i(\omega_o) \cos \theta_i \, d\omega_i} = \frac{\int \left[\int f_r(\omega_o) \cos \theta_o \, d\omega_o\right] \cos \theta_o \, d\omega_o}{\int \int \int f_r(\omega_o) \cos \theta_o \, d\omega_o} = \frac{\int \int \int f_r(\omega_o) \cos \theta_o \, d\omega_o}{\int \int \int f_r(\omega_o) \cos \theta_o \, d\omega_o} = \frac{\int \int \int f_r(\omega_o) \cos \theta_o \, d\omega_o}{\int \int \int f_r(\omega_o) \cos \theta_o \, d\omega_o} = \frac{\int \int \int f_r(\omega_o) \cos \theta_o \, d\omega_o}{\int \int \int f_r(\omega_o) \cos \theta_o \, d\omega_o} = \frac{\int \int f_r(\omega_o) \cos \theta_o \, d\omega_o}{\int \int f_r(\omega_o) \cos \theta_o \, d\omega_o} = \frac{\int f_r(\omega_o) \cos \theta_o \, d\omega_o}{\int \int f_r(\omega_o) \cos \theta_o \, d\omega_o} = \frac{\int f_r(\omega_o) \cos \theta_o \, d\omega_o}{\int \int f_r(\omega_o) \cos \theta_o \, d\omega_o} = \frac{\int f_r(\omega_o) \cos \theta_o \, d\omega_o}{\int f_r(\omega_o) \cos \theta_o \, d\omega_o} = \frac{\int f_r(\omega_o) \cos \theta_o \, d\omega_o}{\int f_r(\omega_o) \cos \theta_o \, d\omega_o} = \frac{\int f_r(\omega_o) \cos \theta_o \, d\omega_o}{\int f_r(\omega_o) \cos \theta_o \, d\omega_o} = \frac{\int f_r(\omega_o) \cos \theta_o \, d\omega_o}{\int f_r(\omega_o) \cos \theta_o \, d\omega_o} = \frac{\int f_r(\omega_o) \cos \theta_o \, d\omega_o}{\int f_r(\omega_o) \cos \theta_o \, d\omega_o} = \frac{\int f_r(\omega_o) \cos \theta_o \, d\omega_o}{\int f_r(\omega_o) \cos \theta_o \, d\omega_o} = \frac{\int f_r(\omega_o) \cos \theta_o \, d\omega_o}{\int f_r(\omega_o) \cos \theta_o \, d\omega_o} = \frac{\int f_r(\omega_o) \cos \theta_o \, d\omega_o}{\int f_r(\omega_o) \cos \theta_o \, d\omega_o} = \frac{\int f_r(\omega_o) \cos \theta_o \, d\omega_o}{\int f_r(\omega_o) \cos \theta_o \, d\omega_o} = \frac{\int f_r(\omega_o) \cos \theta_o \, d\omega_o}{\int f_r(\omega_o) \cos \theta_o \, d\omega_o} = \frac{\int f_r(\omega_o) \cos \theta_o \, d\omega_o}{\int f_r(\omega_o) \cos \theta_o \, d\omega_o} =$$

Reflectance

- Ratio of the incoming and outgoing flux
 - A.k.a. "albedo" (used mostly for diffuse reflection)
- Hemispherical-hemispherical reflectance
 - See the "Energy conservation" slide
- Hemispherical-directional reflectance
 - **□** The amount of light that gets reflected in direction $ω_o$ when illuminated by the unit, uniform incoming radiance.

$$\rho(\omega_{o}) = a(\omega_{o}) = \int_{H(\mathbf{x})} f_{r}(\omega_{i} \to \omega_{o}) \cos \theta_{i} d\omega_{i}$$

Hemispherical-directional reflectance

- Nonnegative
- Less than or equal to 1 (energy conservation)

$$\rho(\omega_{o}) \in [0,1]$$

- Equal to directional-hemispherical reflectance
 - What is the percentage of the energy coming from the incoming direction $ω_i$ that gets reflected (to any direction)?"
 - Equality follows from the Helmholz reciprocity

Albedo

- ◆ fraction of light reflected from a diffuse surface
 - usually refers to an average across the visible spectrum

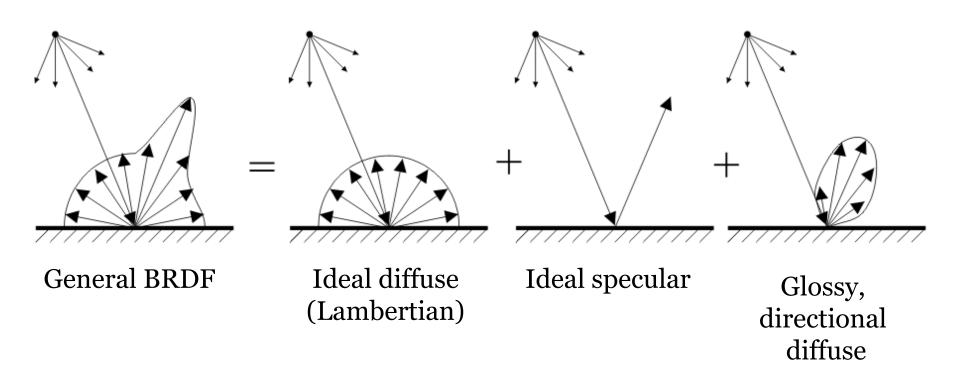


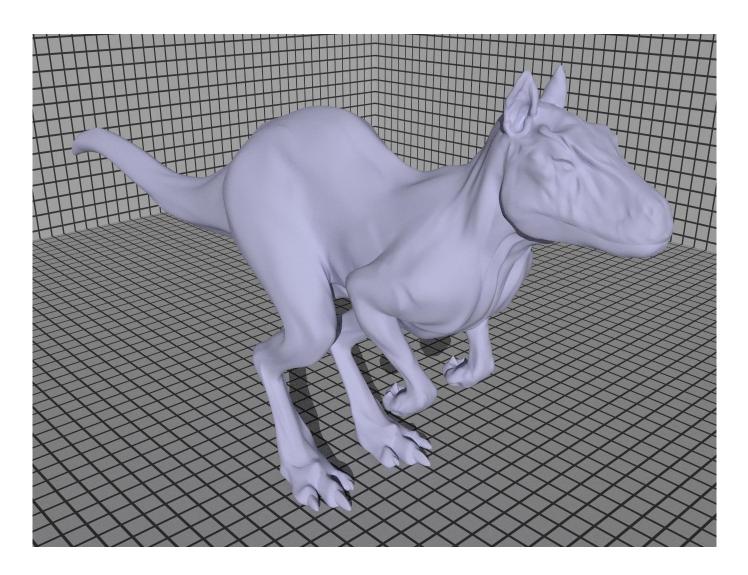
Diffuse albedo and total reflectance measurements

Diffuse albedo and total reflectance measurements			
Jaroslav Křivánek Nov 09, 2009	object / material	diffuse albedo (%)	total reflectance (%) (very approximate)
Procedure briefly described on page 2.	bialetti espresso maker (brand new)	3.2	90
	aluminum foil top	1.2	90
	aluminum foil bottom	2.9	85
	knife blade	1.4	60
	spatula (chrome)	0.9	85
	pizza spatula (scratched)	2.2	60
	rhodes light switch cover - top (coarse finish - aniso)	2.7 / 9.3 *	50
	rhodes light switch cover - bottom (polished)	1.0	70
	chair upholstery	from (6.5, 6, 5.5) to (13, 12, 11)	
	plant leaf	green from (6, 12, 5) to (11 18 8) yellow from (27, 36, 19) to (31, 42, 16)	
	rhodes office desk	(35, 35, 34)	
	plastic cup		
	notebook paper (yellowish)	(89, 80, 71)	
	plate	(83, 81, 71)	
	paper plate	(82, 80, 78)	
	wood	from (50, 30, 19) to (80, 53, 34)	
	rhodes office wall paint	(64, 60, 51)	
	rhodes office door paint	(24, 25, 22)	
	file cabinet (gray paint)	(6.6, 6.6, 6.4)	
	rhodes carpet	(18, 15, 13)	
	dark reddish wood	from (18, 9, 4) to (33, 17, 8)	
	milos's thesis binding	2.8	
	canon lens cap (black plastic)	2.7	
	cornell recycle bin (blue plastic)	(1, 5, 25)	

^{*} viewing along scratches / perpendicular to scratches

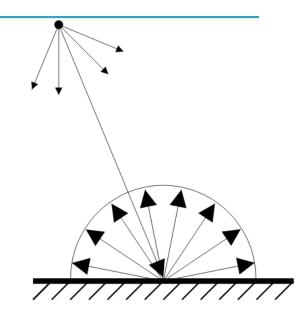
BRDF components





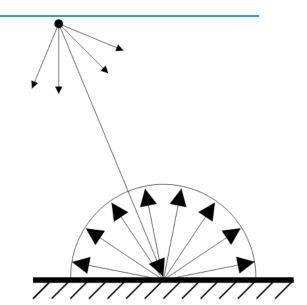
- A.k.a. Lambertian reflection
 - Johann Heinrich Lambert, "Photometria", 1760.





- Postulate: Light gets reflected to all directions with the same probability, irrespective of the direction it came from
- The corresponding BRDF is a constant function (independent of ω_i , ω_o)

$$f_{r,d}(\omega_{\rm i} \rightarrow \omega_{\rm o}) = f_{r,d}$$



Reflection on a Lambertian surface:

$$L_{o}(\omega_{o}) = f_{r,d} \int_{H(\mathbf{x})} L_{i}(\omega_{i}) \cos \theta_{i} d\omega_{i}$$
$$= f_{r,d} E_{\leftarrow}$$

irradiance

- View independent appearance
 - Outgoing radiance L_0 is independent of ω_0
- Reflectance (derive)

$$\rho_d = \pi \cdot f_{r,d}$$

- Mathematical idealization that does not exist in nature
- The actual behavior of natural materials deviates from the Lambertian assumption especially for grazing incidence angles

White-out conditions

Under a covered sky we cannot tell the shape of a terrain

covered by snow





 We do not have this problem close to a localized light source.



Why?

White-out conditions

• We assume sky radiance independent of direction (covered sky) $L_{i}(\mathbf{x}, \omega_{i}) = L^{\text{sky}}$

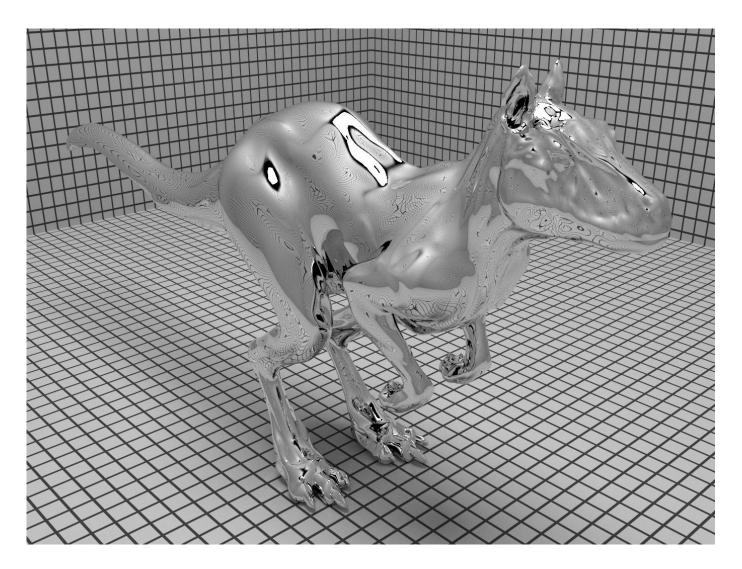
Reflected radiance given by:

$$L_{\mathrm{o}}^{\mathrm{snow}} = \rho_d^{\mathrm{snow}} \cdot L_{\mathrm{i}}^{\mathrm{sky}}$$

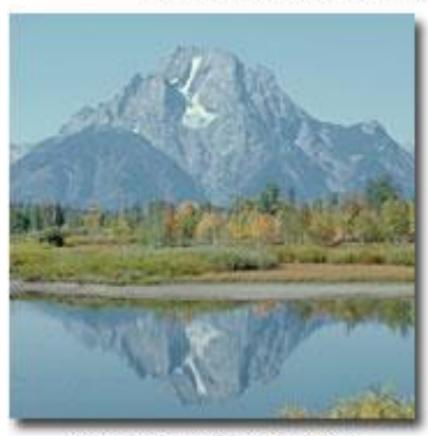
White-out!!!

Ideal mirror reflection

Ideal mirror reflection



Reflections From the Surface of Water



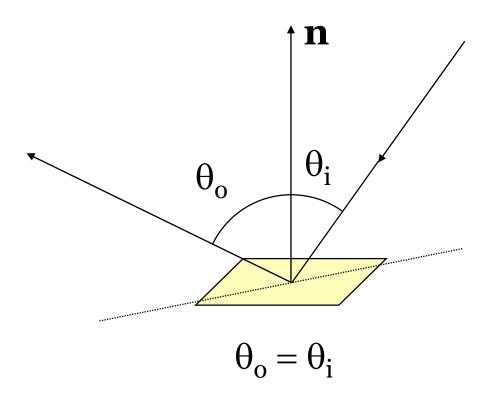
Smooth Water Surface

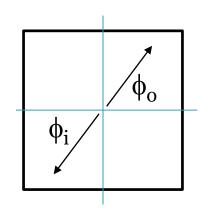


Wavy Water Surface



The law of reflection





$$\phi_{o} = (\phi_{i} + \pi) \bmod 2\pi$$

Direction of the reflected ray (derive the formula)

$$\omega_o = 2(\omega_i \cdot \mathbf{n})\mathbf{n} - \omega_i$$

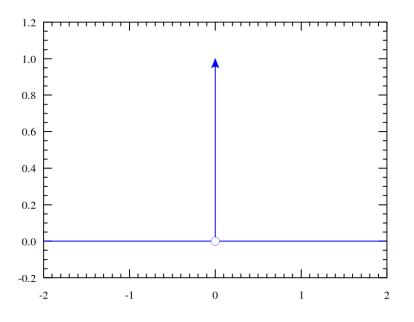
Digression: Dirac delta distribution

Definition (informal):

$$\delta(x) = \begin{cases} +\infty, & x = 0 \\ 0, & x \neq 0 \end{cases}$$
$$\int_{-\infty}^{\infty} \delta(x) \, dx = 1.$$

• The following holds for any *f*:

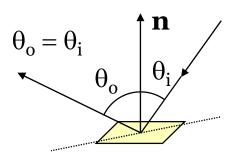
$$\int_{-\infty}^{\infty} f(x)\delta(x) \, dx = f(0)$$



Delta distribution is **not a function** (otherwise the integrals would = 0)

BRDF of the ideal mirror

BRDF of the ideal mirror is a Dirac delta distribution



We want:

$$L_{\rm r}(\theta_{\rm o}, \varphi_{\rm o}) = R(\theta_{\rm i}) L_{\rm i}(\theta_{\rm o}, \varphi_{\rm o} \pm \pi)$$

Fresnel reflectance (see below)

$$f_{r,m}(\theta_{i}, \varphi_{i}; \theta_{o}, \varphi_{o}) = R(\theta_{i}) \frac{\delta(\cos \theta_{i} - \cos \theta_{o}) \delta(\varphi_{i} - \varphi_{o} \pm \pi)}{\cos \theta_{i}}$$

BRDF of the ideal mirror

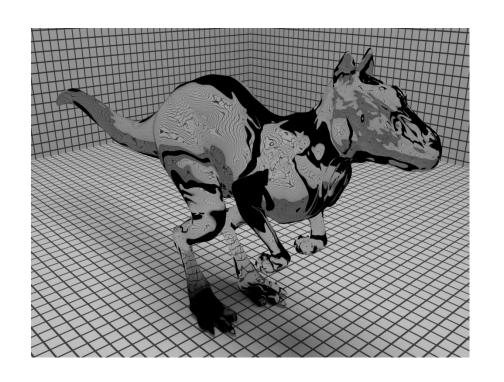
- BRDF of the ideal mirror is a Dirac delta distribution
- Verification:

$$\begin{split} L_{r}(\theta_{o}, \varphi_{o}) &= \int f_{r,m}(.) \ L_{i}(.) \cos \theta_{i} \ d\omega_{i} \\ &= \int R(\theta_{i}) \frac{\delta(\cos \theta_{i} - \cos \theta_{o}) \ \delta(\varphi_{i} - \varphi_{o} \pm \pi)}{\cos \theta_{i}} L_{i}(\theta_{i}, \varphi_{i}) \cos \theta_{i} \ d\omega_{i} \\ &= R(\theta_{i}) L_{i}(\theta_{r}, \varphi_{r} \pm \pi) \end{split}$$



Diego Velázquez, Venus at her Mirror, 1647

Q. Who is Venus looking at in the mirror?



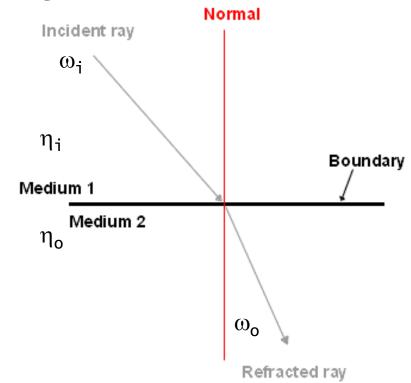


Index of refraction η

- Water 1.33, glass 1.6, diamond 2.4
- Often depends on the wavelength

Snell's law

$$\eta_i \sin \theta_i = \eta_o \sin \theta_o$$

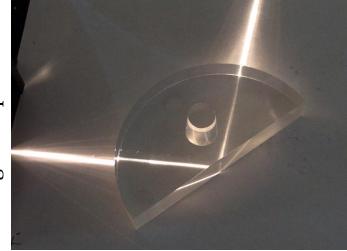


Direction of the refracted ray:

$$\omega_{\rm o} = -\eta_{\rm io}\,\omega_{\rm i} - \left(\eta_{\rm io}\,\cos\theta_{\rm i} + \sqrt{1-\eta_{\rm io}^2(1-\cos^2\theta_{\rm i})}\right)\mathbf{n}$$

$$\eta_{
m io} = rac{\eta_{
m i}}{\eta_{
m o}}$$





Critical angle:

$$\theta_{\mathrm{i,c}} = \arcsin\left(\frac{\eta_{\mathrm{o}}}{\eta_{\mathrm{i}}}\right)$$

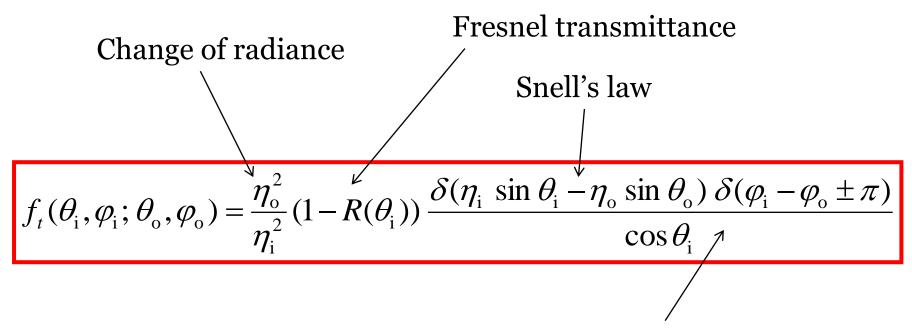
Change of radiance

- Follows from the conservation of energy (flux)
- When going from an optically rarer to a more dense medium, light energy gets "compressed" in directions => higher energy density => higher radiance

$$L_o = L_i \frac{\eta_o^2}{\eta_i^2}$$

BRDF of ideal refraction

BRDF of the ideal refraction is a delta distribution:

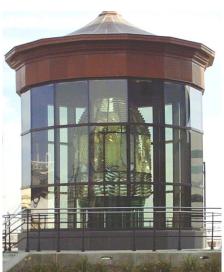


Refracted ray stays in the incidence plane



- Read [frenel]
- Ratio of the transmitted and reflected light depends on the incident direction
 - □ From above more transmission
 - □ From the side more reflection
- Extremely important for realistic rendering of glass, water and other smooth dielectrics
- Not to be confused with Fresnel lenses (used in lighthouses)











From the side

- little transmission
- more reflection

Try for yourself!!!

From above

- little reflection
- more transmission

SHOW VIDEO FROM SKYPE

Dielectrics

$$R_{\rm s} = \left| \frac{n_1 \cos \theta_{\rm i} - n_2 \cos \theta_{\rm t}}{n_1 \cos \theta_{\rm i} + n_2 \cos \theta_{\rm t}} \right|^2$$

$$R_{\rm p} = \left| \frac{n_1 \cos \theta_{\rm t} - n_2 \cos \theta_{\rm i}}{n_1 \cos \theta_{\rm t} + n_2 \cos \theta_{\rm i}} \right|^2$$

$$R = \frac{R_s + R_p}{2}$$

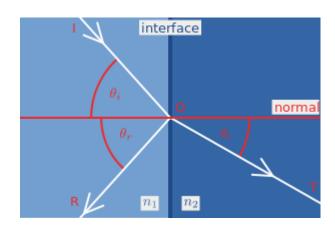
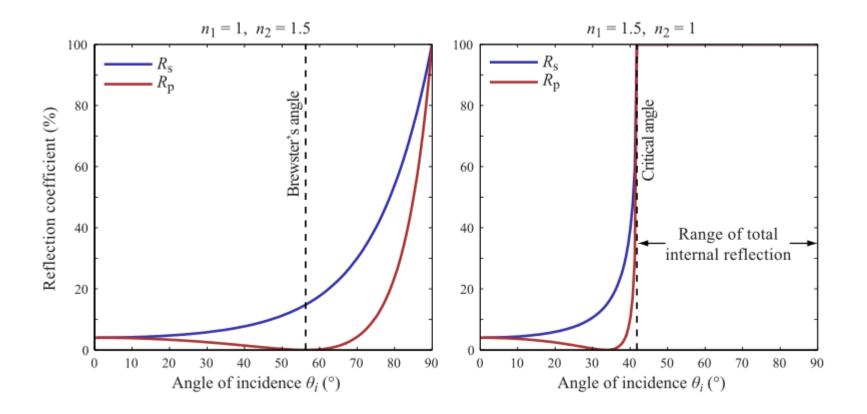


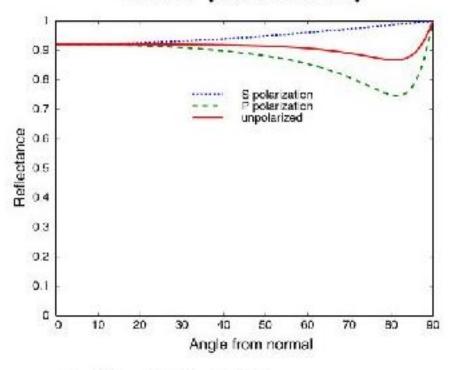
Image: Wikipedia

Dielectrics



Metals

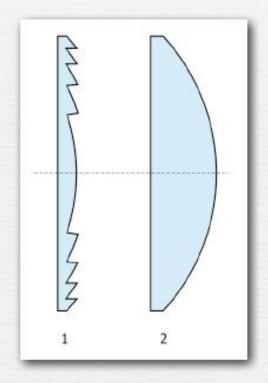
Metal (Aluminum)



Gold F(0)=0.82 Silver F(0)=0.95

Fresnel Lens

- * same refractive power (focal length) as a much thicker lens
- good for focusing light, but not for making images



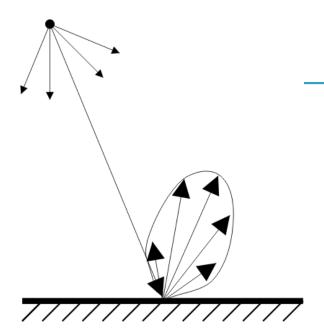


(wikipedia)



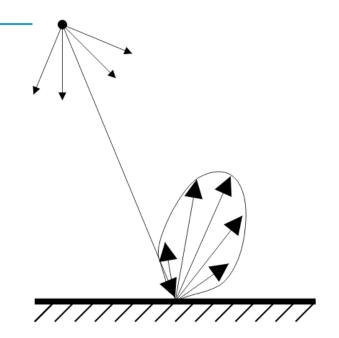
Tyler Westcott, Pigeon Point Lighthouse in light fog, photographed during the annual relighting of its historical 1KW lantern, 2008 (Nikon D40, 30 seconds, ISO 200, not Photoshopped)

Glossy reflection

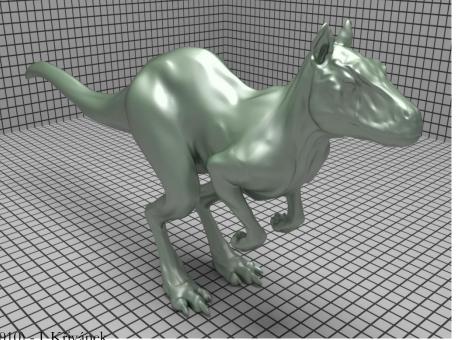


Glossy reflection

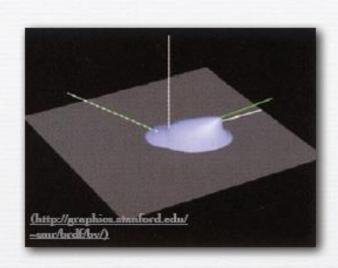
- Neither ideal diffuse nor ideal mirror
- All real materials in fact fall in this category







What unusual material property does this goniometric diagram depict?



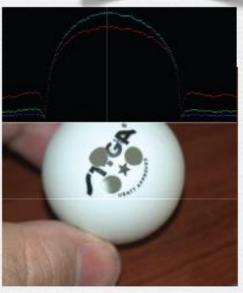


- the maria of the moon is retroreflective and gray
- a diffuse object, lit from the camera's viewpoint, falls off as cos θ

a full moon is roughly lit from the camera's viewpoint



so is a flash photograph



BRDF models

BRDF modeling

BRDF is a model
 of the bulk
 behavior of light Object scale
 when viewing a
 surface from
 distance

BRDF models

□ Empirical Milliscale (a.k.a meso-scale)

- Physically based
- Approximation of measured data

Geometry 100-Texture. bump maps Texels 1 mm 0.1 BRDF 0.01

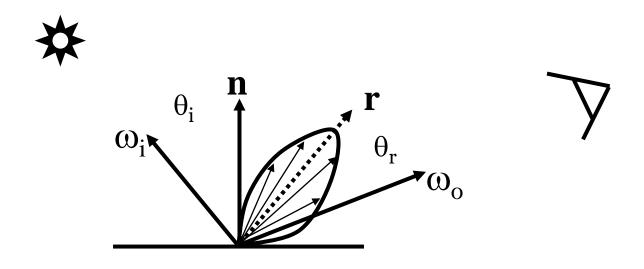
CG III (NPGR010) - J. Křivánek

Microscale

Empirical BRDF models

- An arbitrary formula that takes ω_i and ω_o as arguments
- ω_i and ω_o are sometimes denoted L (Light direction) a V (Viewing direction)
- Example: Phong model
- Arbitrary shading calculations (shaders)

BRDF corresponding to the original Phong shading model



$$f_r^{Phong Orig} = k_d + k_s \frac{\cos^n \theta_r}{\cos \theta_i}$$

Problems: breaks symmetry & energy conservation

Physically-plausible Phong BRDF

 Modification to ensure reciprocity (symmetry) and energy conservation

$$f_r^{\text{Phong modif}} = \frac{\rho_d}{\pi} + \frac{n+2}{2\pi} \rho_s \cos^n \theta_r$$

Energy conserved when

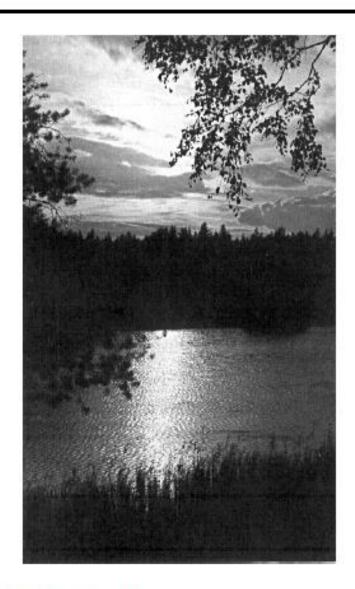
$$\rho_d + \rho_s \le 1$$

 It is still an empirical formula (i.e. it does not follow from physical considerations), but at least it fulfills the basic properties of a BRDF

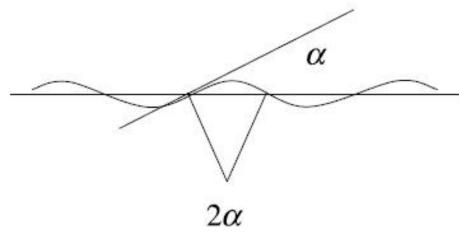
Physically-plausible BRDF models

- E.g. Torrance-Sparrow / Cook-Torrance model
- Based on the microfacet theory

Reflection of the Sun from the Sea



Minnaert, Light and Color in the Outdoors, p. 28



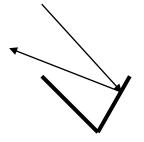
SHOW PICS OF VLTAVA RIVER

- Analytically derived
- Used for modeling rough surfaces (as the Phong model)
 - Corresponds more closely to reality than Phong
 - Derived from a physical model of the surface microgeometry (as opposed to "because it looks good"approach used for the Phong model)

Assumes that the macrosurface consists of randomly oriented microfacets



- We assume that each microfacet behaves as an ideal mirror.
- We consider 3 phenomena:



Reflection



Masking



Shadowing

Microfacet theory [Cook et Torrance 1982]

A perfect mirror

- Reflection in a single direction
- Outgoing light visible surface normal aligned with the half vector
- Half Vector: $H = \frac{L+V}{\|L+V\|}$

<u>Aggregation of micro-mirrors</u> (micro-facets)

- Each micro-mirror have a micro-normal
- How many micro-mirror have their micro-normal aligned so that H = N?
- Statistical distribution: Normal Distribution Function (NDF)

Fresnel term

Geometry term

Models shadowing and masking

$$f = \frac{F(\theta_i)G(\omega_i, \omega_r)D(\theta_h)}{4\cos(\theta_i)\cos(\theta_r)}$$

 $\frac{h}{h}$ distribution

Microfacet

Part of the macroscopic surface visible by the light source

Part of the macroscopic surface visible by the viewer

- SHOW GGX
- PBRWORKFLOW
- SUBSTANCE DESIGNER

THE DISNEY "PRINCIPLED" BRDF

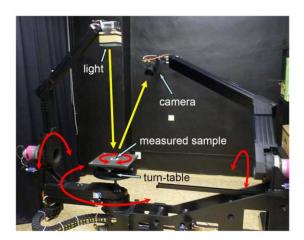
Approximation of measured data

- We can fit any BRDF model to the data
- Some BRDF models have been specifically designed for the purpose of fitting measured data, e.g. Ward BRDF, Lafortune BRDF
- Nonlinear optimization required to find the BRDF parameters

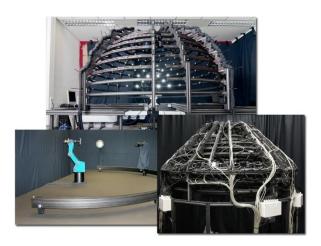
BRDF measurements – Gonio-reflectometer







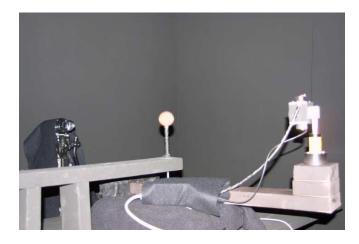
UTIA



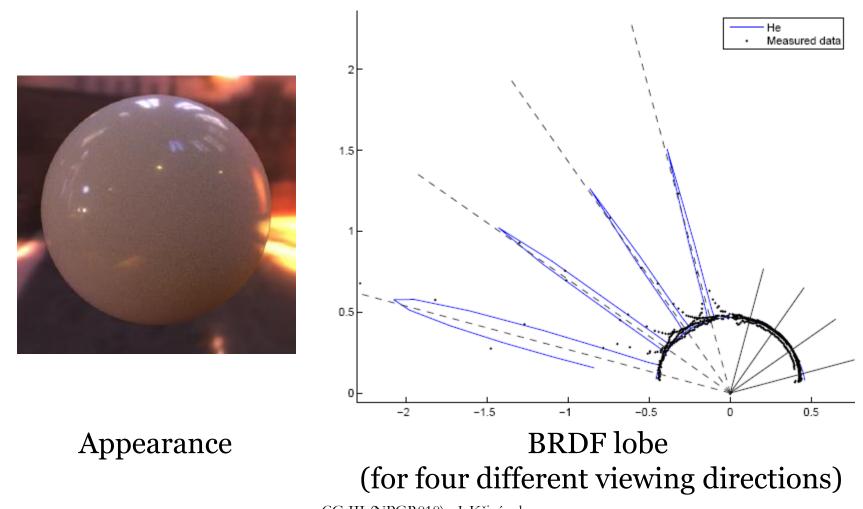
University of Bonn

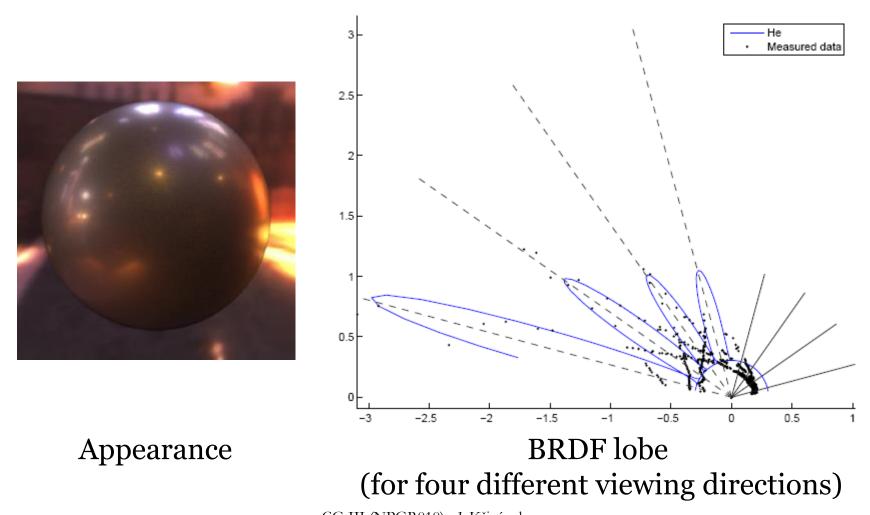
Measured Material

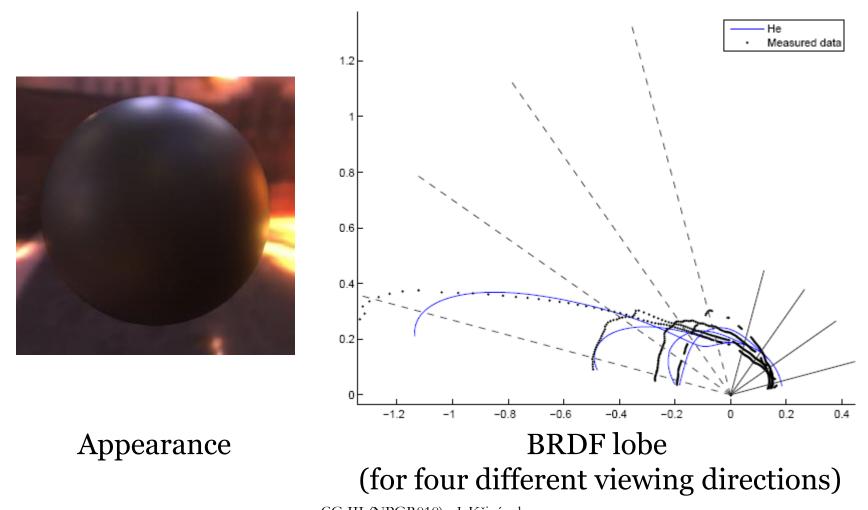
- Techniques for speeding measurements
 - Mirrors
 - Objects coated by the material:
 - Sphere [<u>Matusik et al 2003</u>]
 - Cylinders [Ngan et al 2005]

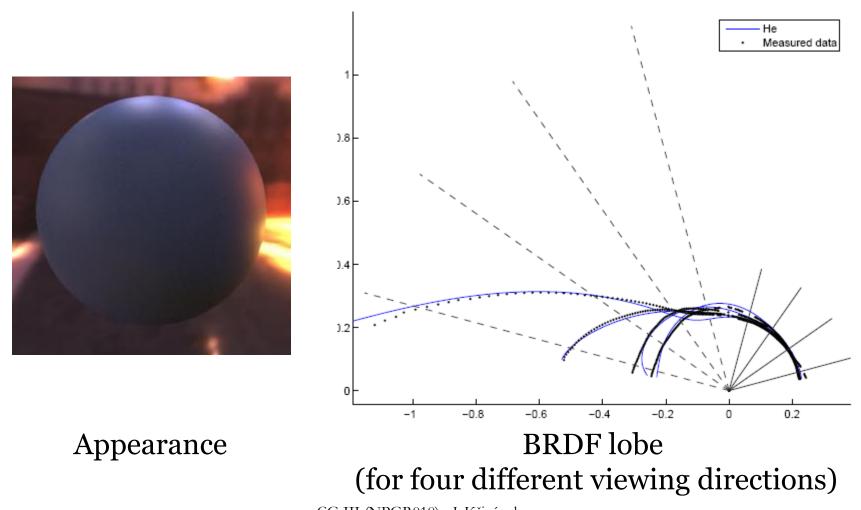


Matusik et al 2003





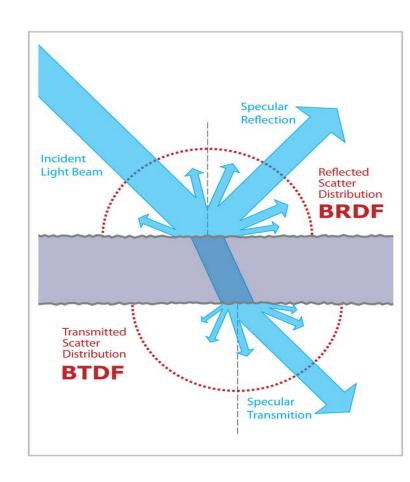




BRDF, BTDF, BSDF: What's up with all these abbreviations?

BTDF

- Bidirectional transmittance distribution function
- Described light transmission
- \blacksquare **BSDF** = BRDF+BTDF
 - Bidirectional scattering distribution function



SBRDF, BTF

SV-BRDF ... Spatially Varying BRDF

 BRDF parameters are spatially varying (can be given by a surface texture)

BTF ... Bidirectional Texture Function

- Used for materials with complex structure
- As opposed to the BRDF, models even the meso-scale



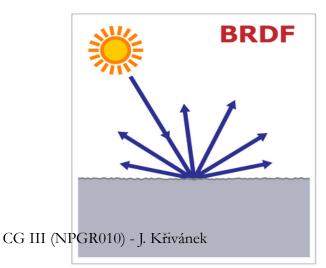
BSSRDF

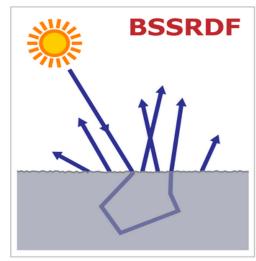
BRDF

- Light arriving at a point is reflected/transmitted at the same point
- No subsurface scattering considered

BSSRDF

- Bi-directional surface scattering reflectance distribution function
- Takes into account scattering of light under the surface





BSSRDF

Sub-surface scattering makes surfaces looks "softer"





BRDF BSSRDF

BSSRDF













BRDF

BSSRDF

References

- PBR manuals from substance
- ••••